

APPLICATION  
FOR  
UNITED STATES LETTERS PATENT

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PATENT APPLICATION

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SPECIFICATION

TO ALL WHOM IT MAY CONCERN:

Be it known that Kevin J. Knopp of 55 Curzon's Mill Road, Newburyport, MA 01950, Daryoosh Vakhshoori of 10 Rogers Street, Apt. 205, Cambridge, MA 02142, Peidong Wang of 225 Davis Road, Carlisle, MA 01741 and Donald L. McDaniel of 92 Prescott Street, North Andover, MA 01845, have invented certain improvements in MONOLITHIC SEMICONDUCTOR LIGHT SOURCE WITH SPECTRAL CONTROLLABILITY, of which the following description is a specification.

KK/AHURA3.CVR

MONOLITHIC SEMICONDUCTOR LIGHT SOURCE  
WITH SPECTRAL CONTROLLABILITY

1. Reference To Pending Prior Patent Application

5           This patent application (i) claims benefit of  
pending prior U.S. Provisional Patent Application  
Serial No. 60/440,115, filed 01/15/03 by Kevin Knopp et  
al. for MONOLITHIC SEMICONDUCTOR LIGHT SOURCE WITH  
SPECTRAL CONTROLLABILITY (Attorney's Docket No. AHURA-3  
10       PROV) and (ii) is a continuation-in-part of pending  
U.S. Patent Application Serial No. 10/632,779, filed  
08/01/03 by Daryoosh Vakhshoori et al. for SYSTEM FOR  
AMPLIFYING SIGNALS (Attorney's Docket No. AHURA-1),  
which two patent applications are hereby incorporated  
15       herein by reference.

2. Field Of The Invention

          This invention relates to optical systems in  
general, and more particularly to systems for  
20       amplifying optical signals.

### 3. Background Of The Invention

#### 3.1 In General

5           Dense wavelength-division multiplexing (DWDM) is  
currently the preferred method for satisfying bandwidth  
demand for fiber-optic long-haul transport in  
telecommunication systems. As the optical data signal  
travels through the fiber, however, fiber  
10 nonlinearities, fiber loss, and amplified spontaneous  
emission (ASE) all act to degrade the signal-to-noise  
ratio of the data signal. As a result, the optical  
signal needs to be periodically amplified and  
eventually electrically regenerated so as to maintain  
15 the signal integrity.

The design of an economical DWDM network has to  
consider performance versus cost for all of the network  
elements such as transmitters, amplifiers,  
regenerators, add/drop nodes, receivers, etc. To save  
20 expense on the amplifiers, for example, the length of  
the amplifier span should be as long as possible.  
Extended amplifier span, however, results in high ASE

accumulation from low input to amplifiers, and/or large nonlinear effects due to the use of high launch power. This degradation in turn demands more frequent optical-to-electrical-to-optical (OEO) regeneration. A typical 40 channel DWDM system using Erbium-doped fiber amplifiers (EDFA's) generally has an amplifier span spacing of about 80 km and OEO regeneration distances of around 500-600 km.

Currently, OEO regeneration is responsible for a much larger percentage of overall system cost than amplifiers. It is, therefore, desirable to extend the regeneration distance wherever possible.

Raman fiber amplifier technologies have emerged as a highly promising building block to allow DWDM transmission for distances greater than 1500 km without OEO regeneration. This is particularly important inasmuch as the majority of data traffic on a telecommunications network typically has a destination distance which exceeds 1000 km.

Raman fiber amplifiers generally use the transmission fiber itself as the gain medium. Thus, the signal passing through the fiber is amplified as it

propagates. Because of their distributed nature, Raman amplifiers present several significant advantages over EDFA technologies:

(1) Since the Raman amplification makes the fiber partially transparent, a high signal-to-noise ratio can be maintained over multiple span distances.

(2) For the same reason, the nonlinear effects can be significantly reduced since the maximum signal power in the fiber can be significantly reduced.

(3) The Raman gain profile of optical fiber is much broader and smoother than that of EDFA's. As a result, the combination of several pump laser wavelengths can provide overall gain profiles as broad as near 100 nm with less than 1 dB gain ripple, thus reducing the gain ripple and tilting effects generally associated with EDFA's.

(4) Inline EDFA's typically operate in saturation mode where the gains of the amplifier for individual wavelength channels are a function of total input signal power. As a result, when an optical channel is added or dropped from the fiber, the gains for all of the other channels change, causing network transients,

distortions and misbalances. By contrast, Raman amplifiers typically work in a linear mode where the gain of each channel is independent of all of the other channels. Thus, dynamic wavelength adds/drops in a Raman system have less of an effect on overall system performance.

Raman-assisted transmission generally compares favorably to EDFA-only systems, leading to better system quality factors, longer amplifier spans, and hence longer DWDM transmission before the need for OEO regeneration.

One evolving application area of Raman amplifiers, beyond the traditional long-haul transmission application discussed above, is in the hybrid fiber coaxial cable (community antenna) TV (HFC-CATV) industry. HFC-CATV, using subcarrier multiplexing (SCM) and multilevel quadrature amplitude modulation (QAM) technology, generally requires >50 dB carrier-to-noise ratio and high suppression of inter-modulation, second order and third order distortions, which generally calls for high optical power and low noise accumulation. Currently, this is

typically achieved by employing high output power EDFA's (up to 25 dBm) and limiting span spacing (typically 30-40 km) and amplifier stages. However, by using distributed Raman amplification, it is possible, due to the low noise figure (NF) and in-fiber Raman amplification, to extend the span spacing, add amplifier stages and lower input power without significantly compromising system performance. However, applications of Raman amplifiers in the CATV industry are currently impaired by cost.

Improvements in Raman amplification would also have advantageous applications in a wide range of instrumentation and imaging applications.

### 3.2 Principles Of Raman Amplification

The principles of Raman amplification in fiber are based on the process of stimulated Raman scattering (SRS). When an optical beam of frequency  $\omega_p$  is injected into, and propagates along, an optical fiber, a small fraction (typically  $10^{-6}$ ) of the incident photons are scattered by the molecules to lower-frequency ( $\omega_s < \omega_p$ ) states while, at the same time, the

molecule makes a transition between vibrational states.

The incident light acts as a pump to generate the frequency

down-shifted ( $\omega_s$ ) light, which is sometimes called

5 Stokes waves. If a signal at the frequency  $\omega_s$  is coincident with the pump beam (at frequency  $\omega_p$ ) in the fiber, the signal will be amplified by the Raman scattering-induced Stokes waves (also at frequency  $\omega_s$ ).

10 One outstanding feature of fiber Raman amplifiers is that the Raman gain profile of standard fused silica fiber is very broad due to the amorphous nature of the glass. Typically, the Raman gain increases nearly linearly from the pump frequency towards a maximum at about 13.2 THz (100 nm) and then falls off fairly sharply. For example, if a high power 1450 nm laser is  
15 injected into a 40 km standard single mode fiber such as Corning SMF-28<sup>TM</sup> fiber, the Raman gain profile will have a maximum near 1550 nm, with a usable gain bandwidth of ~30 nm (see Fig. 1).

20 The magnitude of the Raman gain in optical fiber depends on the respective compositional doping elements. The normalized gain spectral shape, however,



is much less sensitive to glass composition for most fibers typically used.

In the first order approximation, the Raman gain increases nearly linearly, in dB, with increasing pump power. Nearly 10 dB of Raman gain is typical for 500 mW of pump power injected into 40 km of Corning SMF-28™ fiber. The upper limit of realistically useful Raman gain is generally limited by the double Rayleigh scattering process. At that upper limit, the Rayleigh back scattering causes multiple reflections of both the ASE and the signal, thus causing performance degradation of the transmission. Double Rayleigh scattering becomes prominent as the Raman gain reaches above 15 dB.

Due to the fact that the Raman gain profile is determined by the pump laser wavelength, the Raman gain spectrum can be tailored in shape and width by selecting the appropriate pump laser wavelength spectrum. For telecommunication applications, it is common to combine a number of high power diode lasers, each with a different wavelength, to collectively yield a broad and flat gain profile so as to accommodate the

transmission window of interest. To construct a 100 nm bandwidth Raman amplifier, up to 8 pump wavelengths, ranging from 1430 nm to 1520 nm, are needed for the amplification of signals in the 1530 nm to 1620 nm band with less than 1 dB gain ripple. The 1 dB gain ripple is due in part to the fine and sharp structures near the peak of the gain profile shown in Fig. 1.

One significant characteristic of Raman amplifiers is that Raman amplification is effective only if the signal beam has the same polarization as that of the pump. To obtain a polarization-insensitive Raman amplifier, two diode lasers, with orthogonal polarization, are generally used for each pump wavelength. Alternatively, another approach to solve this issue is to use various polarization scrambling techniques. However, current polarization scrambling techniques are generally relatively costly and bulky, and have unproven reliability.

Another important issue for distributed Raman amplification is the relative intensity noise (RIN) transfer from the pump laser to the signal. Raman scattering, due to its fast response time, causes

amplitude noise in the pump lasers to be proportionally transferred to the gain fluctuations. As is schematically shown in Fig. 2, when a noise-free signal beam propagates along the Raman amplified transmission fiber, the signal data set experiences a time-dependent amplification. As a result of this phenomena, the output signal beam carries amplitude noise.

The noise transfer from pump laser to the signal beam depends on the pump geometry employed.

More particularly, if the pump propagates in the direction opposite to that of the signal, the signal beam experiences the gain through its entire traveling time in the fiber, and the RIN of the pump laser is then effectively averaged over the travel time. For a fiber length of 20 km, the signal beam traveling time is about 100 microseconds. The high frequency RIN components, typically above 1 MHz, are substantially insensitive to the signal transmission quality (Fig.3). This suppression of the RIN transfer from pump to signal is one of the main reasons that "backward pumping" remains the most popular scheme for Raman amplification in telecommunication systems.

On the other hand, when a forward pump scheme is employed so as to provide a co-propagating pump and signal, the average of the pump RIN is determined only by the walk-off time between the signal and pump generated by dispersion of the fiber. The RIN transfer from pump to signal remains effective for much higher frequency components, as shown in Fig. 3. The RIN of the pump lasers must then generally be limited to  $<-150$  dB/Hz. This requirement is often difficult to achieve for the commonly-used frequency-stabilized Fabry-Perot lasers. To achieve such low RIN, distributed feedback (DFB) lasers have generally been used for forward pumping applications. A disadvantage of using DFB lasers as a Raman pump, however, is that the narrow linewidth of a DFB laser causes significant Brillouin back-scattering at a power level much lower than that needed for the Raman pump. As a result, linewidth broadening techniques need to be applied to suppress the Brillouin scattering while keeping the RIN within the required range.

When multiple high power diode lasers are used as the Raman pumping source, nonlinear interactions

between the various pumps becomes an important design consideration. When the frequencies of the pump lasers vary over 100 nm, the pumps at high frequency can effectively amplify the pumps at lower frequencies (see Fig. 4), causing nonlinear power evolution of the pumps inside the fiber. In addition, four-wave-mixing between pumps can create side bands with frequencies extending into the signal band. This causes an excessive noise floor for certain signal channels.

Generally, distributed Raman amplifiers are currently associated with high cost because of their sophisticated design, expensive high power diode lasers and complex packaging. More fundamentally, technical limitations such as pump-pump nonlinear interactions and gain ripple are inherently associated with the use of multiple high power diode lasers to provide a relatively broad and flat gain profile.

#### 4. Summary Of The Invention

The present invention provides solutions to a number of the challenges described above.

More particularly, in one form of the invention, there is provided a system for amplifying optical signals comprising: an optical fiber for carrying the optical signals; a high power broadband light source; and a connector for introducing the high power broadband light source into the optical fiber as a Raman pump so as to induce Raman amplification of the optical signals within the fiber.

In another form of the invention, there is provided a method for amplifying optical signals comprising: introducing a high power broadband light source into an optical fiber carrying the optical signals so that the high power broadband light source acts as a Raman pump so as to induce Raman amplification of the optical signals within the fiber.

And in another form of the invention there is provided a spectrally filtered high power broadband light source comprising a spectrally filtered amplified spontaneous emission (ASE) generated from an optical component.

## 5. Brief Description Of The Drawings

These and other objects and features of the present invention will be more fully disclosed or rendered obvious by the following detailed description of the preferred embodiments of the invention, which is  
5 to be considered together with the accompanying drawings wherein like numbers refer to like parts and further wherein:

Fig. 1 is a schematic diagram showing the  
10 normalized Raman gain spectrum of standard single mode fiber, at a pump wavelength of 1450 nm;

Fig. 2 is a schematic diagram showing distributed Raman amplification using forward pumping;

Fig. 3 is a schematic diagram showing the RIN  
15 transfer spectrum for a co-pumped and counter-pumped Raman amplifier with 10 dB of gain;

Fig. 4 is a schematic diagram showing the power evolution of pump diode lasers along the fiber path;

Fig. 5 is a schematic diagram showing the  
20 simulated Raman gain shape achieved using (i) six discrete pump wavelengths, and (ii) two broadband light sources;

Fig. 6 is a schematic diagram showing depolarizers for long and short coherence light sources;

Fig. 7 is a schematic diagram showing the reduction of FWM achieved in a Raman amplifier pump using (i) discrete pump wavelengths, and (ii) a broadband ASE source;

Fig. 8 is a schematic diagram showing a broadband ASE Raman pump source;

Fig. 9 is a schematic diagram illustrating how multiple ASE sources can be superimposed so as to form a composite ASE spectrum for Raman pumping;

Fig. 10 is a schematic diagram illustrating a first preferred embodiment for forming a broadband ASE source;

Fig. 11 is a schematic diagram illustrating a second preferred embodiment for forming a broadband ASE source;

Fig. 12 is a schematic diagram illustrating a third preferred embodiment for forming a broadband ASE source;



Fig. 13 is a schematic diagram illustrating a fourth preferred embodiment for forming a broadband ASE source;

5 Fig. 14 is a diagram showing the use of a discrete seed and booster to generate high power ASE;

Fig. 15 is a schematic diagram illustrating a fifth preferred embodiment for forming a broadband ASE source;

10 Fig. 16 is a schematic illustration showing a booster power module (BPM) simulated transverse mode shape of an asymmetric optical confined ridge waveguide;

15 Fig. 17 is a schematic illustration showing a finite element simulation of the temperature distribution of a booster waveguide;

Fig. 18 is a schematic diagram of a MMI power combiner;

Fig. 19 is a schematic illustration of a wet etched InP based booster amplifier ridge waveguide;

20 Fig. 20 is a schematic diagram of a holographic lithography system;

Fig. 21 is a schematic diagram showing a broadband light source configuration with seed wavelength control based on thin-film filters;

Fig. 22 is a schematic diagram showing simulated transmission of a multicavity thin-film notch filter used for seed wavelength control;

Fig. 23 is a schematic diagram showing measured performance obtained using a discrete seed and booster as shown in Fig. 21 for ASE generation; and

Fig. 24 is a schematic diagram showing a measured ASE spectrum at 100mW of output power from the booster waveguide shown in Fig. 21.

## 6. Detailed Description Of The Preferred Embodiments

### 6.1 The Use Of Amplified Spontaneous Emission (ASE) As A Raman Pump Source

In accordance with one aspect of the present invention, a high power broadband light source is used as a high power Raman pump source to facilitate the amplification of optical signals.

In one preferred form of the invention, the high power broadband light source is generated from spectrally filtered amplified spontaneous emission (ASE) from various semiconductor or fiber sources.

5        The use of a high power broadband light source as a Raman pump source has inherent performance advantages in the areas of gain ripple and flatness, nonlinear pump-to-pump interactions, pump-to-signal interactions, and in the methods of depolarization.

#### 10        6.1.1 Gain Ripple And Flatness

To extend the amplification bandwidth in Raman amplifiers, it is a straightforward approach to multiplex a number of pump lasers (each with a  
15        different pump wavelength) to reach the desired gain bandwidth. The excited gain spectrum is a convolution of the pump spectrum and the Raman gain shape shown in Fig. 1. For each pump wavelength, the Raman gain profile (Fig. 1) shows a sharp feature near the peak of  
20        the Raman gain. The severity of this feature depends to some extent on the composition of the fiber, and hence on the fiber type. To eliminate this ripple,

pump lasers must be spaced such that the frequency difference between adjacent pumps is less than the bandwidth of the ripple. Given the fact that high power diode lasers are expensive, as is the packaging of multiple diodes, the number of diode lasers used, and the distribution of their wavelength spacing, has to be designed so as to achieve maximum bandwidth, and minimum gain tilt and ripple, within feasible cost. Fig. 5 illustrates the gain profile of a typical design using 6 discrete pump wavelengths distributed across 80 nm. The gain ripple of 0.5 dB is observed. Further reduction of the gain ripple can generally be achieved only if the pump wavelength spacing is reduced to less than 2 nm. Thus, an unfeasibly large number of pump lasers are needed to cover the 80 nm bandwidth.

Significantly, however, if a broadband high power ASE source is used as the Raman pump instead of the multiple discrete wavelength lasers, a large reduction in gain ripple is observed. The solid curve in Fig. 5 illustrates the results when two broadband pump sources are used to yield a nearly perfectly smooth gain profile. The smoothness of the gain ripple is a direct

result of the physical convolution "like" process  
between the pump source spectrum and the Raman response  
function of the optical fiber. The overall flatness of  
the achieved gain can be controlled by selecting the  
proper spectral profiles (i.e., wavelength and power  
distribution) of the broadband pump sources.

#### 6.1.2 Depolarization

As noted above, Raman gain is highly polarization  
dependent. Amplification of the signals is essentially  
only realized along the same polarization direction as  
the polarization of the pump. To reduce the  
polarization-dependent gain, the solution is to provide  
a depolarized pump source. In current Raman pump  
modules, this is generally accomplished in one of two  
ways.

The most common approach is to use two  
semiconductor lasers for each wavelength desired, each  
with orthogonal linear polarizations. This technique  
also allows the total pump power to be distributed  
amongst two lasers rather than one. However, inasmuch  
as each laser ages independently, there is concern

about the degradation of the polarization-dependent gain over the life of the amplifier.

The second approach is often used when the laser output power of a single laser diode is sufficiently high to supply Raman gain for both polarizations. In this alternative approach, a depolarizer is used to create two orthogonal linear polarizations. This depolarizer may be a passive depolarizer comprising a long length of optical fiber (e.g., ~10 m), where the single linear polarization state of the high power laser is split into two orthogonal linear components, delayed, and then recombined into one beam. To obtain two independent orthogonally-polarized beams, it is important that the delay length should be greater than the coherence length of the source or an elliptical polarization state will be formed when recombined. Thus, the long length of the optical fiber depolarizer is necessary when depolarizing a semiconductor laser with an optical fiber depolarizer so as to provide the appropriate delay for the long coherence length of the semiconductor laser.

Significantly, the coherence length of broadband ASE is inherently shorter than a semiconductor laser by about 3 orders of magnitude (e.g., it is only ~1 mm). This is because the incoherence of the source allows a much shorter delay length. Consequently, the depolarizer for broadband ASE can be constructed from a compact series of bulk optical components. Fig. 6 is a schematic diagram of exemplary optical elements, and a pictorial illustration of the polarization state, for depolarizing short and long coherence light sources. The small size of the optical elements and their spacing allows them to be readily integrated into the package of the high power broadband Raman pump source.

#### 6.1.3 Nonlinear Interactions And Beat Noise

As the optical power injected into fiber increases, nonlinear optical effects, such as Self-phase modulation (SPM), cross-phase modulation (XPM), and four-wave mixing (FWM), can become an important source of noise. The nonlinear optical interaction can originate from the signal channel as well as from the pump lasers. The relative importance

of these effects depends on the particular system design parameters such as power per channel, channel spacing, the total number of channels and fiber dispersion. For multi-wavelength pumped Raman amplifiers, one particularly important nonlinear effect is four-wave mixing between pump lasers. This can be especially detrimental as the amplifier bandwidth approaches the Raman gain peak shift (i.e., ~100 nm).

When  $n$  lasers with discrete laser frequencies ( $\omega_{P1} \dots \omega_{Pn}$ ) are used for pumping the optical fiber, FWM generates side bands at  $\omega_{FWM} = \omega_{Pi} + \omega_{Pj} - \omega_{Pk}$ , with  $i, j, k = 1, 2 \dots n$ . With all of the  $i, j, k$  combinations possible, the FWM side bands are distributed between frequencies of  $\omega_{P1} - \Delta_P$  and  $\omega_{Pn} + \Delta_P$ , where  $\Delta_P = (\omega_{Pn} - \omega_{P1})$  is the frequency range of the pump lasers. The strength of the FWM sidebands at  $\omega_{FWM} = \omega_{Pi} + \omega_{Pj} - \omega_{Pk}$  is proportional to  $|P_i P_j^* P_k|^2$ . For broadband Raman amplifiers, where  $\Delta_P$  approaches 100 nm, the FWM sidebands on the low frequency (long wavelength) side can fall within the signal window of the frequencies of the amplifier. This effect can be observed in forward, as well as backward, pumped Raman amplifier configurations. In



backward pumped configurations (i.e., with signal and pump counter-propagating), the FWM parasitic signal is redirected into the signal direction through Raleigh scattering. If the parasitic FWM signal falls within the receiver bandwidth of a practical signal channel, the quality of the transmission within that channel is seriously degraded.

The system quality as a whole is limited by the worst case of all the signal channels.

In connection with the present invention, it has been found that overall system performance can be much improved if the pump source has a continuous broadband distribution. This is because when the total optical power is unchanged, the FWM sidebands are redistributed over a large number of signal channels, rather than where the FWM side bands are being concentrated over a few signal channels. Fig. 7 illustrates the reduction of FWM achieved in a Raman amplifier pump with a broadband ASE source (see the schematic "b" in Fig. 7) as compared to a Raman amplifier pumped with discrete wavelengths (see the schematic "a" in Fig. 7).

#### 6.1.4 Raman Gain Beating

In addition to the degradation of an amplifier's noise characteristics due to nonlinear phenomena, linear mechanisms can also be responsible for degradation. One such linear mechanism is Raman gain beating which is caused by a coherent beat frequency located between longitudinal modes of a Fabry-Perot laser cavity. For a 1 mm laser cavity length, the mode spacing is approximately 3 angstroms. This corresponds to a 40 GHz coherent beat frequency. This coherent beating is particularly detrimental to the noise figure in the forward (i.e., pump and signal co-propagation) Raman amplifier configuration. Significantly, in the case of a broadband ASE pump source, the lack of coherence of the source substantially completely eliminates Raman gain beating.

### 6.2 High Power Broadband Semiconductor ASE Source

#### 6.2.1 Spectrally Filtered High Power

#### Broadband ASE Source In General

The broadband light source used as the Raman pump source can be generated from any light which has a sufficiently broad and intense emission spectrum. Such light sources can be formed, for example, from amplified spontaneous emission (ASE) of rare earth doped optical fiber, planar waveguides, or semiconductor optical amplifiers. Further examples are spectrally broadened multimode semiconductor lasers or multiorder cascaded Raman lasers. These latter examples (i.e. spectrally broadened multimode semiconductor lasers and multiorder cascaded Raman lasers) have previously been used as Raman pump sources, but with an emphasis on their use for suppressing stimulated Brillouin scattering and, significantly, the spectral broadening is generally limited to no more than a couple of nanometers.

This document will hereinafter concentrate on methods and apparatus for providing a high power broadband light source using amplified spontaneous emission (ASE) from semiconductor optical amplifiers. However, it will be appreciated by those skilled in the art that these same methods and apparatus can be

applied in principle to ASE generated from other laser gain medium.

Fig. 8 illustrates a schematic block diagram of a broadband ASE source in combination with spectral filtering to achieve a desired spectral distribution for the Raman pump. Gain profile shaping can be effected by wavelength filtering, within or outside the active devices, in a dynamic or static fashion. Thin-film filters or Bragg gratings can be used for such wavelength filtering.

One of the most promising and economical solutions for making high power broadband ASE sources is high power semiconductor devices with a specifically designed waveguide structure and facet coating.

The broad optical spectrum can be provided by a single ASE source or a superposition of multiple narrower bandwidth (e.g., 3-40 nm) ASE sources. These narrower bandwidth ASE sources can be multiplexed together in a continuous or discontinuous fashion as illustrated in Fig. 9 so as to form a composite ASE source. In this manner, gain flatness control can be achieved through the control of the total pump

spectrum, where total pump spectrum control is in turn achieved through the control of the contribution of the relative intensity of each narrower bandwidth ASE source.

5           A high power broadband ASE source can also be used for purposes other than Raman amplifiers, e.g., as light sources for general instrumentation (including for example fiberoptic gyros), imaging (including, for example, medical imaging), and semiconductor analysis  
10 applications. These applications can benefit since relatively high power can be achieved without the complication of laser speckle resulting from its temporal coherence; however, the waveguide nature of the source provides spatial coherence, thus allowing  
15 spatial manipulation of the output as efficiently as a laser beam. Additionally, the relative intensity noise of this source has been shown to be as good as the best semiconductor laser.

#### 20           6.2.2 Semiconductor Embodiments In General

This section describes the semiconductor chip design, fabrication, and packaging considerations for

realizing such a device. The semiconductor material system used depends to a large extent on the wavelength of the desired application. Among others, material systems such as AlAs, GaAs, InP, GaP, InGaAs, InGaAsP, InAlGaAs, and GaN can be used.

The basic principle of device operation is the amplification of a seed spectrum of amplified spontaneous emission (ASE) along the length of a semiconductor waveguide containing one or more active regions which are biased above transparency. The manner in which the seed light is generated and shaped (i.e., filtered), the number of waveguides used, the number of sections the waveguides are comprised of, the optical bandgap and electrical bias of those sections, and the method of multiplexing multiple waveguides, all have various preferred embodiments which will be described below.

#### 6.2.2.1 First Embodiment

Fig. 10 is a schematic diagram of a semiconductor die 100 used in a first preferred embodiment. The die 100 consists of a serial connection of a wavelength

seed section 103 and a power booster or power amplification section 106 formed along a semiconductor waveguide 109.

5       The wavelength seed section 103 preferably comprises multiple subsections 103A, 103B, 103C, etc. formed along the semiconductor waveguide 109. Three subsections 103A, 103B, 103C are shown in Fig. 10; however, it should be appreciated that this number is merely exemplary and more or less than this number of  
10       wavelength seed subsections may be used. The gain profile within each subsection 103A, 103B, 103C, etc. is chosen so as to provide ASE in a particular wavelength range. The gain profiles can be defined in each subsection 103A, 103B, 103C, etc. by such  
15       techniques as epitaxial regrowth or quantum well intermixing. The quantum well blocks of these subsections are designed to provide a region of high gain with, for example, 3-10 quantum wells.

20       A high reflectance mirror 112 is used to capture and redirect the portion of seed light traveling away from the power booster section 106. The spectral profile of this mirror 112 is designed to provide the

desired nominal ASE spectrum at the input of the power booster section 106. This high reflectance mirror 112 can be defined through thin film coating of the cleaved semiconductor facet or by incorporating a distributed Bragg reflector along the waveguide. Each wavelength seed subsection 103A, 103B, 103C, etc. has an independent electrical contact to allow dynamic tailoring of the seed light spectrum prior to launching into the power booster section 106. The output power of the wavelength seed section 103 can range from 1 to 20 mW, although it is not limited to this range.

The power booster section 106 is designed to amplify the broad spectrum (20-100 nm) of ASE seed light and generate power in excess of 500 mW. This can be accomplished through the use of a long waveguide section 109A which is optimized for low loss rather than high gain. Reducing the number of quantum wells to the range of 1 to 5, reducing optical confinement in p-doped cladding, and increasing the confinement factor in n-doped cladding (which has lower free carrier absorption loss) will all reduce the loss. Additionally, the quantum wells must provide gain



across the entire wavelength range of the seed light.

This can be accomplished through chirping of the thickness of the quantum wells in the vertical direction. For example, the upper quantum well

5 provides shorter wavelength gain while the lower two quantum wells provide longer wavelength gain.

An angled waveguide 109B is used at the output of the power booster section 106, followed by an antireflection coating 115 on the semiconductor facet.

10 This combination is used to eliminate feedback into the power booster section 106 and to prevent distortion of the broadband spectral profile from Fabry-Perot interference.

As is the case for all of the embodiments  
15 discussed herein, the output will be highly linearly polarized because of the polarization dependence of the quantum well gain or, in the case of bulk active region, excess loss of TM over TE mode. If two equal components of linear orthogonal polarization are  
20 desired for applications such as Raman amplifiers, the construction described in Fig. 6(b) can be used.

The advantages of the construction shown in

Fig. 10 include: full semiconductor integration, serial multiplexing, compatibility with dynamic spectral flattening, and reduced packaging complexity, among others.

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#### 6.2.2.2 Second Embodiment

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Fig. 11 is a schematic diagram of a semiconductor chip 200 and optical train 203 used in a second preferred embodiment. Although multiple chips can be used, this embodiment will be described in the context of a single chip 200 comprising an array of parallel waveguides 206, where the array comprises a plurality (e.g., 2 to 10) of parallel waveguides 206A, 206B, 206C, etc. The gain profile (i.e., peak wavelength and shape) of each waveguide 206A, 206B, 206C, etc. is chosen so as to provide the ASE output in a particular wavelength range (e.g., 3-30 nm).

20

The gain profiles can be defined within each waveguide 206A, 206B, 206C, etc. by employing such techniques as epitaxial regrowth, quantum well intermixing or other techniques known in the art. The spectral width and intensity of the ASE emitted from each waveguide 206A, 206B, 206C, etc. can be tailored

through the design of the active region, the length of the waveguide, and active adjustment of the current injected into each waveguide. The quantum well block of each waveguide is designed to provide a region of high gain with, for example, 3-10 quantum wells, along the first 0.3  $\mu\text{m}$  to 1 mm length of the waveguide. The remainder of the waveguide is optimized for low loss rather than high gain so as to amplify the ASE seed light and generate power in excess of 200 mW. To achieve low loss, the number of quantum wells is preferably reduced to the range of, for example, 1 to 5, and the doping in the waveguide cladding can be reduced. A high reflectance mirror 209 is provided at one end of the waveguide, and angled waveguides 212A, 212B, 212C, etc. used at the output, followed by a facet antireflection coating 215. This combination is used to eliminate feedback into the power booster and prevent distortion of the broadband spectral profile from Fabry-Perot interference.

The waveguide design of this second embodiment differs from the first embodiment (Fig. 10) discussed above in that each waveguide 206A, 206B, 206C, etc.

only needs to produce power in a narrower spectral range (e.g., 3-30 nm). The power and spectral width of each waveguide 206A, 206B, 206C, etc. are then multiplexed using the optical train 203 contained within the hermetically sealed package.

The optical train 203 comprises a polarization multiplexer 218 for each pair of waveguides 206A, 206B, 206C, etc., followed by a wavelength multiplexer port 221 for each pair of multiplexers 218. Fig. 11 illustrates this multiplexing principle for 4 waveguides using two polarization multiplexers 218 and a two-port wavelength multiplexer 221.

The advantages associated with the construction shown in Fig. 11 include: redundancy, compatibility with dynamic spectral flattening, compatibility with cooler-less operation, and a lower optical power requirement per waveguide, among others.

#### 6.2.2.3 Third Embodiment

Fig. 12 is a schematic diagram of a semiconductor chip 300 and optical train 303 used in a third preferred embodiment. The die 306 consists of a

wavelength seed section 309 which is power multiplexed  
by a multiplexer 312 into a long low loss power  
amplification (or booster) waveguide 315. Wavelength  
seed section 309 preferably comprises a plurality of  
5 wavelength seeds 309A, 309B, 309C, etc. Both the seed  
light waveguides 309A, 309B, 309C, etc. and the power  
booster waveguide 315 are designed for broadband ASE  
emission, just as in the first embodiment (Fig. 10)  
discussed above. A high reflectance mirror is provided  
10 for each of the seed waveguides 309A, 309B, 309C, etc.  
These mirrors may be independent of one another, or  
they may be different sections of a single mirror, such  
as is shown in Fig. 12 with the high reflectance mirror  
318. The reflectivity profiles of the high reflectance  
15 mirror for each seed waveguide 309A, 309B, 309C, etc.  
are optimized to provide the correct seed light profile  
for control of the output ASE spectrum. The power  
booster waveguide 315 includes an angled end 321 and an  
anti-reflectance coating 324 at its output end.  
20 Spectrum function controls such as tilt can be achieved  
through the appropriate mix of seed light functions.

The advantages of the construction shown in

Fig. 12 include: redundancy, and reduced control circuit complexity, among others.

#### 6.2.2.4 Fourth Embodiment

5            Fig. 13 is a schematic diagram of a semiconductor die 400 and optical train 403 used in a fourth preferred embodiment. The semiconductor die 400 consists of an array of, for example, 2 to 10, parallel waveguides 406A, 406B, 406C, etc., each with a  
10           narrowband wavelength reflector (e.g., 3-10 nm) to define the seed light bandwidth for each waveguide 406A, 406B, 406C, etc. A plurality of discrete reflectors, each formed independent of the others, may be provided; or the reflectors may be different  
15           sections of a single reflector, such as is shown in Fig. 13 with the reflector 409. The reflector (as in all of the foregoing embodiments) can be formed, for example, by thin-film deposition, an etched semiconductor distributed Bragg reflector (DBR), or an  
20           abutted glass planar light wave guide/grating. Fig. 13 illustrates the use of a planar light wave circuit grating to form the reflector 409. The attributes of

the power waveguides 406A, 406B, 406C, etc. are substantially the same as disclosed in the second embodiment (Fig. 11) discussed above. The outputs of the waveguides 406A, 406B, 406C, etc. are wavelength  
5 combined using a thin-film edge-filter multiplexer 412. The multiplexer 412 is preferably formed using a glass substrate 415 with a series of patterned edge-filters 418 deposited by thin film deposition.

The advantages of the construction shown in  
10 Fig. 13 include: compatibility with dynamic spectral flattening, and lower optical power requirement per waveguide, among others.

#### 6.2.2.5 Fifth Embodiment

15 Fig. 14 is a schematic diagram of a high power spectrally filtered ASE source 500 which comprises a fifth embodiment of the present invention. ASE source 500 comprises a discrete seed 505 and booster 510 which are used to generate high power ASE. More  
20 particularly, an isolator 515 is positioned between seed 505 and booster 510, and a mirror 520 is positioned between isolator 515 and booster 510. A

lens 525 is positioned between seed 505 and isolator 515, a lens 530 is positioned between mirror 520 and booster 510, and a lens 540 is positioned at the output of booster 510. In this construction, spectrally filtered ASE light is produced in seed 505, it is passed through lens 525 and isolator 515, reflected off mirror 520, passed through lens 510 and into booster 510, where it is amplified, and then passed out lens 540.

#### 6.2.2.6 Sixth Embodiment

Fig. 15 is a schematic diagram of a spectrally controllable light source device 600 which comprises a sixth embodiment of the present invention. Spectrally controllable light source 600 consists of a waveguide seed section 605 which is coupled by a broadband power combiner 610 into a long single-mode high-power "booster" waveguide 615. Waveguide seed section 615 comprises a plurality of wavelength seeds 605A, 605B, 605C, 605D, etc. Both the seed light waveguides 605A, 605B, 605C, 605D, etc. and the power booster waveguide 610 are designed for broadband ASE emission, just as in



the first embodiment (Fig. 10) discussed above. A high reflectance mirror is provided for each of the seed waveguides 605A, 605B, 605C, 605D, etc. These mirrors may be independent of one another, or they may be  
5 different sections of a single mirror, such as is shown in Fig. 15 with the high reflectance mirror 620. The reflectivity profiles of the high reflectance mirror for each seed waveguide 605A, 605B, 605C, 605D, etc. are optimized to provide the correct seed light profile  
10 for control of the output ASE spectrum. The power booster waveguide 615 includes an angled end 625 and an anti-reflectance coating 630 at its output end. Spectrum function controls such as tilt can be achieved through the appropriate mix of seed light functions.

15 Preferably, each one of the wavelength seeds 605A, 605B, 605C, 605D, etc. generate a low power optical seed signal which differ in center wavelength from one another and are approximately 5 nm in spectral width. The low power optical seed signals, which are  
20 preferably in the range of 1-20mW, are power combined by broadband combiner 610 into long single-mode high-power "booster" waveguide 615 which amplifies the seed

signals to higher optical power signals, which are preferably greater than 200 mW. The optical output has a single spatial mode and is linearly (TE) polarized, preferably greater than 20 dB. Additionally, the output will exhibit a relative-intensity noise performance rivaling that of a distributed-feedback (DFB) laser ( $< -140$  dB/Hz). Through varying the bias current to each of N seed amplifier waveguides 605A, 605B, 605C, 605D, etc., the spectral output can be dynamically tailored.

Several preferred embodiments of the present invention are described herein below which relate to the waveguide seed section 605 and power booster amplifier waveguide 615, the broadband N x 1 power combiner 610, and the method of seed-wavelength control are described in more detail hereinbelow.

#### SEED & Power Booster Amplifier Waveguides

The wavelength seed section 605 of the device 600 is comprised of a parallel array of active semiconductor waveguides 605A, 605B, 605C, 605D, etc.

The gain profile within each waveguide is engineered to provide ASE in a particular wavelength range when electrically biased above transparency. It is important to have a high modal gain (both  $g$  &  $\Gamma$ ) to allow efficient generation of ASE and coupling of the ASE into the waveguide mode for amplification. The desired design parameter optimization needed for seed amplifier waveguide 605A, 605B, 605C, 605D, etc. is similar in nature to that needed for conventional semiconductor optical amplifiers. Preferably, a high reflecting narrowband filter 635 is used to capture, spectrally shape, and redirect the fraction of ASE traveling in the waveguide away from the power booster. The spectral profile of mirror 620 is designed to provide the desired center wavelength and spectral width of the ASE spectrum at the input of the power booster waveguide 615. Each wavelength seed section has an independent p-side electrical contact so as to allow dynamic tailoring of the seed light spectrum. The output power of the wavelength seed section 605 preferably ranges from 1 to 20 mW.

The power booster section 615 is designed to amplify the ASE light from seed waveguides 605A, 605B, 605C, 605D, etc. which generate power in excess of 200 mW. The design optimization needed for the power booster 615 is complimentary in nature to that required for high power, i.e., greater than 400mW, telecommunication lasers. See, for example, (1) Garbuzov D., et al., (2002). 14xx nm DFB InGaAsP/InP pump lasers with 500 mW CW output power for WDM combining. Optical Fiber Communications Conference, Anaheim, CA; and (2) Tsukiji N., et al., (2001). Recent progress of high power 14xx nm pump lasers. SPIE ITcom on Active and Passive Optical Components for WDM Communication, Denver, CO. It is desirable to use a waveguide optimized for low loss rather than high gain. Waveguides with a modal loss of less than  $2 \text{ cm}^{-1}$  are generally utilized. This is accomplished by reducing the number of quantum wells, reducing the optical confinement factor, and utilizing asymmetric confinement where the modal overlap is larger over the n-doped cladding than the p-doped cladding. Additionally, a long cavity reduces the devices voltage

drop and allows a lower dopant concentration to be used for reduction of free carrier absorption loss. For example, this cavity may extend several millimeters.

Furthermore, the quantum wells provide gain across  
5 the entire wavelength range of the seed light signals.

In a preferred embodiment of the present invention, this is accomplished by chirping the thickness of the quantum wells in the growth direction. For example, the upper quantum well provides shorter wavelength gain  
10 while the lower two quantum wells provide longer wavelength gain.

Referring still to Fig. 15, and in a preferred embodiment of the present invention, an angled waveguide 625 is used at the output of the power  
15 booster followed by an antireflection coating 630 on the semiconductor facet. This combination is used to reduce feedback into the power booster to less than -60dB and thus prevent distortion of the broadband spectral profile from Fabry Perot interference. The  
20 output will be highly linearly polarized because of the polarization dependence of the quantum well gain.

Preferably, angled waveguide has an angle of about 8°-13°.

High power ASE is achieved by using discrete seed waveguides 605A, 605B, 605C, 605D, etc. together with booster amplifier waveguide 615. Device 600 is able to provide ASE power output in excess of 250mW with a spectral full-width at half-maximum of 20 nm.

#### Power Combiner

Power combiner 610 is used rather than a wavelength combiner to guide seed light to booster waveguide amplifier 615 for at least two reasons. One reason is the tremendously challenging complexity for fabrication of a spectrally flat-top and broadband wavelength multiplexer, such as a multicavity Arrayed Waveguide Grating (AWG). Integrated wavelength multiplexing is also unfeasible due to concerns of optical feedback to the seed waveguides as well the large surface area requirements.

Many applications rely on wavelength combiners due to the inherent 1/N splitting loss of a power combiner. This intrinsic loss has minimal impact on device 600 as

the power booster will be operating in a power saturated regime. A total input power of only several milliwatts to booster waveguide 615 is needed to deliver in excess of 200 mW of output power. The use of power combiner 610, such as a multimode interferometer (MMI) coupler, is ideal for device 600 in that the MMI has relaxed requirements on the excess loss, broad spectral performance, and provides a high return loss. See, for example, Okamoto, K. (2000). Fundamentals of Optical Waveguides. San Diego, Academic Press. Low loss can be achieved in the interference region of MMI though either (1) quantum-well intermixing, (2) epitaxial regrowth, or (3) electrical bias to transparency. See, for example, (1) Holonyak, N. (1998). "Impurity-induced layer disordering of quantum-well heterostructures: discovery and prospects." IEEE J. Tpcs. Quantum Electron. 4(4) 584-594; (2) Kudo K., et al. (2000). "1.55  $\mu\text{m}$  wavelength-selectable microarray DBF-LDs with monolithically integrated MMI combiner, SOA, and EA-modulator." IEEE Photon. Technol. Lett. 12(3); and (3) Hamamoto K., et al., (2002). High-power with low electric power consumption 1.45  $\mu\text{m}$  active multi-mode

interferometer laser diode for fiber amplifier applications. Optical Fiber Communications Conference, Anaheim, CA.

5

Seed Wavelength Control

A host of technologies are available in the fabrication of a wavelength control mechanism 635. Referring still to Fig. 15, and in a preferred embodiment of the present invention, an approximately  
10 5 nm narrow-band high-reflecting mirror can be created through incorporation of an etched multicavity Bragg reflector along seed waveguide ridge 605A, 605B, 605C, 605D, etc. The multicavity design can be achieved with properly-designed phase masks, which are  
15 holographically imprinted on the waveguide directly through standard lithography methods. The pattern transfer is preferably achieved through inductively coupled plasma reactive ion etching process.

Referring now to Fig. 26, and in preferred  
20 embodiment of the present invention, wavelength control mechanism 635 for wavelength seeds 605A, 605B, 605C, 605D, etc. comprises a combination of a series of



multicavity narrow-band notch filters 640A, 640B, 640C, 640D, etc. and high reflectivity feedback mirrors 645A, 645B, 645C, 645D, etc. Multicavity narrow-band notch filters 640A, 640B, 640C, 640D, etc. are disposed at a 45° angle relative to mirrors 645A, 645B, 645C, 645D, etc., respectively. In this approach, thin film coatings disposed on mirrors 645A, 645B, 645C, 645D, etc. are configured to create a 5 nm flat-top transmission peak.

In a preferred embodiment of the present invention, integrated semiconductor device 600 is capable of generating over 200 mW of fiber coupled power across a spectral range of 1400-1500 nm with 4 or more spectral controls of the emission profile. Each of the spectral controls has 5 nm resolution. This preferred embodiment of the present invention relies on multicavity thin-film filters 640A, 640B, 640C, 640D, etc. for assembly on a micro-optical bench. Specific steps to create this preferred embodiment of the present invention are discussed hereinbelow.

A first step comprises amplifier waveguide design and growth. This step involves determining the appropriate epitaxy structure through simulation and experiment to provide suitable broadband gain, and high power. A single non-integrated booster and seed waveguide are demonstrated.

A second step comprises integrated coupler design. This step involves the design of an MMI active/passive (4 x 1) power combiner for integration with the seeds and booster waveguides. Optical isolation, broadband performance, excess loss, and fabrication methods are simulated.

A third step comprises integrated coupler growth and fabrication. This step involves the growth, fabrication, and characterization of an (4 x 1) MMI active/passive coupler.

A fourth step comprises seed wavelength control. This step encompasses the exploration of various technologies for creating the required narrow-band reflector. Source demonstration may rely on thin-film deposited multi-cavity flat-top 5 nm FWHM bandpass filters.

A fifth step comprises integration, assembly, and characterization. This step involves taking the results of the previous steps and integrating for demonstration and characterization on a micro-optical bench. Power, Spectral Controllability, and Relative Intensity Noise (RIN) are characterized.

A fifth step comprises analysis and optimization. This final step involves systematic study of the results and preparation of fully-integrated sources.

#### Amplifier Waveguide Design & Growth

While a full rate-equation analysis is needed to precisely predict and determine the expected amplifier waveguide performance, the dependence of the design parameters for the seed and booster waveguides can be illustrated through consideration of power conservation. It can be shown that the output ASE power from a self-generating seed amplifier waveguide is proportional to,

$$P_{ASE}^{Seed} \propto \beta \left( \frac{I}{l} \right) \frac{e^{\Gamma g l}}{g}, \quad (1)$$

where  $\beta$  is the spontaneous emission factor,  $\Gamma$  is the optical confinement factor,  $g$  is the material gain,  $I$  is the injected current, and  $l$  is the seed's length. Large modal gain and a high spontaneous emission factor are desirable. For the booster waveguide, the limiting maximum power is given by,

$$P_{ASI}^{Booster} \propto \frac{IV_g \eta - P_{out}^{spon} - P_{heat}^{auger}}{\alpha_{total} \Delta l}, \quad (2)$$

where  $\eta$  is the internal quantum efficiency,  $P_{out}^{spon}$  is the optical power from spontaneous emission,  $P_{heat}^{auger}$  is the power dissipated from nonradiative recombination,  $V_g$  is the active region bandgap voltage,  $I$  is the injected current, and  $l$  is the incremental (saturated) length of the booster. This equation shows that minimization of the total loss, rather than high gain, is desired.

To facilitate on chip integration and eliminate the potential need for epitaxial regrowth, the booster waveguide structure can also be used for the seed waveguide structure by increasing the length of the seed. However, this increases die length, and thus effects power consumption, yield, and ultimately cost.

To achieve ASE emission and gain over an extended bandwidth (100 nm), a chirped quantum well design is employed. This is accomplished through varying the thickness of the quantum wells in the growth direction.

5 For example, the upper quantum well provides shorter wavelength gain while the lower two quantum wells provide longer wavelength gain. A solid model will be used for gain curve simulations.

10 As can be observed from Equation 2, modal loss in the amplifier waveguide is an important design parameter. Great care is taken to properly optimize this parameter. The impact of reducing doping concentration on voltage should also be considered. A technique has been developed to achieve an asymmetric  
15 confinement factor. Asymmetric confinement is used to reduce the mode's overlap with the heavily absorptive p-doped region. Booster amplifier waveguides having less than  $2 \text{ cm}^{-1}$  (total loss) can be achieved using this technique. This technique will further be  
20 optimized in a preferred embodiment of the present invention so as to reduce active amplifier waveguide losses for our proposed device to below  $1 \text{ cm}^{-1}$ .

Referring now to Fig. 16, and in a preferred embodiment of the present invention, there is shown a simulated transverse mode shape 650 of an asymmetric optical confined ridge waveguide 655 of booster waveguide 615 (Figs. 15 and 21).

Referring now to Fig. 17, an extremely important design consideration is thermal management. Often the first limits observed for output power are due to thermal roll over. Finite element techniques may be used to simulate and design the structure's thermal impedance. Looking at Fig. 3, there is shown a temperature distribution 660 for booster waveguide 615 (Figs. 15 and 21). The calculated thermal impedance is greater than  $7^{\circ}/W$  for a 4 mm device.

#### Integrated Coupler Design

An MMI power combiner will be used to guide the light from the seed waveguides to the booster waveguide. MMIs have the unique properties of low insertion loss, large optical bandwidth, compact size, polarization insensitivity, low cross talk, and forgiving fabrication tolerances. (See, for example,

Okamoto, K. (2000). Fundamentals of Optical Waveguides.

San Diego, Academic Press.) A design schematic of a

typical MMI power combiner 665 is shown in Fig. 18.

Using guided mode propagation analysis, (see Soldano,

5 L.B., et al. (1995). "Optical multimode interference

devices based on self-imaging: principles and

applications." J. Lightwave Technol. 13:615-627) the

dimensions of the MMI as shown in Fig. 18 are chosen to

satisfy self-imaging. The influence of waveguide loss

10 on coupler performance are extensively parameterized.

This result together with the outcome of the

fabrication considerations of the step comprising the

integrated coupler growth and fabrication determine the

final MMI design.

15 Several substeps are performed to complete the

integrated coupler design. These substeps include

simulation/calculation using BPM, FDTD, and analytic

techniques of the excess loss, return loss to seed and

booster, spectral dependence of the coupling

20 coefficient, and output mode shape. The substeps also

comprise parameterization of the effect of waveguide

loss and finalization of dimensions and layer structure

using considerations from the step of the integrated coupler growth and fabrication.

#### Integrated Coupler Growth & Fabrication

5           The MMI coupler 665 will be grown in the InP/InGaAsP material system using a MOCVD. Coupler 665 is preferably fabricated using conventional wafer processing techniques. Coupler 665 is fabricated using InP-based materials through optical lithography and  
10           wet/dry etching processes. Referring now to Fig. 19, there is shown a wet-etched InP based ridge waveguide 670 in a SEM micrograph.

          The interference region of the MMI 665 must have low loss. This presents challenges in achieving the  
15           integration of the active seed waveguides 605 and booster waveguides 615 with power combiner 610, such as MMI 665. There are two approaches for achieving low loss. These include quantum-well intermixing, see Holonyak, N. (1998). "Impurity-induced layer  
20           disordering of quantum-well heterostructures: discovery and prospects." IEEE J. Sel. Tpcs. Quantum Electron. 4(4):584-594, and electrical bias to transparency, see



Hamamoto K., et al., (2002). High power with low electric power consumption 1.45  $\mu$ m active multi-mode interferometer laser diode for fiber amplifier applications. Optical Fiber Communications Conference, Anaheim, CA.

The selection of the approach is made through analysis of the simulation results of the integrated coupler design together with the results of initial intermixing experiments.

Intermixing can be used for spatial bandgap tuning of multiquantum well structures, see, for example, Si, S.K., et al., (1998). "Area selectivity of InGaAsP-InP multiquantum-well intermixing by impurity-free vacancy diffusion." IEEE J. Sel. Tpcs. Quant. Elect. 4(4) 619-623. Impurity-free vacancy diffusion (IFVD) benefits from low scattering loss, see Si, S.K., et al., (1998). "Area selectivity of InGaAsP-InP multiquantum-well intermixing by impurity-free vacancy diffusion." IEEE J. Sel. Tpcs. Quant. Elect. 4(4) 619-623. Vacancy intermixing can be achieved through implantation of double-charged phosphorus ions (P++) in the layers above the quantum well active region. See, for

example, Paquette, M. et al. (1998). Blueshifting of InGaAsP-InP laser diodes using a low energy ion-implantation technique." IEEE J. Sel. Tpcs. Quant. Elect. 4(4): 741-745. Point defects are generated that are able to thermally diffuse and contribute to intermixing when annealed. The bandgap of the resulting intermixed material shifts to higher energy by more than 80 nm, i.e., near 1480 nm. The intermixed material exhibits similar photoluminescence intensity to that of the non-implanted material. Lasers with excellent slope efficiency and threshold have been fabricated using intermixed material. See, for example, Paquette, M. et al. (1998). Blueshifting of InGaAsP-InP laser diodes using a low energy ion-implantation technique." IEEE J. Sel. Tpcs. Quant. Elect. 4(4): 741-745; and Yu, S.F., et al. (1998). "Semiconductor lasers using diffused quantum-well structures." IEEE J. Sel. Tpcs. Quant. Elect. 4(4): 723-735. This method of vacancy diffusion is utilized for shifting the bandgap in the interference region of the MMI to avoid optical absorption.

Several substeps are preferably performed during integrated coupler growth and fabrication. One substep is fabrication of waveguide lasers with intermixed material. This is followed by evaluation of the internal loss and the internal quantum efficiency. A freeze fabrication approach may also be used.

#### Seed Wavelength Control

Referring now to Figs. 15 and 20, and in a preferred embodiment of the present invention, narrow-band, high-reflecting mirror 620 is created by incorporating a multicavity Bragg reflector etched along the ridge of seed waveguide 605A, 605B, 605C, 605D, etc. The multicavity design is achieved with a properly-designed phase mask, holographically imprinted on the waveguide 605A, 605B, 605C, 605D, etc. through standard lithography methods. The pattern transfer can be achieved through an inductively-coupled-plasma reactive-ion-etching process.

Looking at Fig. 20, there is shown a holographic lithography technique 675. A Karl Suss MA6 lithography

system is fitted with a near field holographic adapter to create holographic lithography technique 675.

5       The 0 beam 680 and -1 beam 685 are used to create interference patterns 690 on waveguides 605A, 605B, 605C, 605D, etc. The 0/-1 order principle is advantageous for fine-pitch applications that require suppression of unwanted orders. In this geometry, incident light 695 is diffracted partially into the -1 order 685. Self-interference between the -1 order 685 and the undiffracted zero order beam 680 creates an interference pattern 690 with a pitch equal to the phase mask pitch. This approach is advantageous over conventional +1/-1 order phase mask as +1 order beam can degrade the grating formation, and hence influence its optical characteristics.

10

15

Referring now to Fig. 21, and in a preferred embodiment of the present invention, holographic grating technique 675 is implemented for "on-chip" wavelength control for further scaling of the number of seed guides 605. This relies on the use of external thin-film filters 640A, 640B, 640C, 640D, etc. for wavelength control of seeds 605A, 605B, 605C, 605D,

20

etc., respectively. Dielectric notch filters 640A, 640B, 640C, 640D, etc. and high reflecting feedback mirrors 645A, 645B, 645C, 645D, etc. are used in combination with one another, respectively.

5           The multi-cavity and high reflective thin films can be deposited by an Ion Tech Spector ion beam sputtering system. An optical monitoring system ensures accurate coatings to meet the technical requirements. Proper glass substrate ensures athermal  
10 properties of the coating.

          Looking at Fig. 22, there is shown simulated transmission 700 of a multicavity thin notch filter 640A, 640B, 640C, 640D, etc. used for seed wavelength control. Multicavity thin notch filters 640A, 640B,  
15 640C, 640D, etc. are designed as a narrow band filter about 5nm wide and centered at 1450 nm.

          Several substeps are preferably performed for creating seed wavelength control. These substeps include the evaluation of the holographic imprinting  
20 technique for etching of multicavity semiconductor Bragg gratings, the design and deposit thin-film filters for off-chip wavelength control, and the

provision of prototype thin-film wavelength control of a single seed waveguide.

Integration, Assembly, & Characterization

5           Integration and assembly of device 600 occurs after (1) amplifier waveguide design and growth, (2) integrated coupler design, (3) integrated coupler growth and fabrication, and (4) seed wavelength control. Seed array 605 is first fabricated with MMI  
10   coupler 610 and output of MMI 610 is characterized for power, mode shape, spectral distribution, and RIN. Information from these measurements is then used to feedback and iterate the process where required. Booster 615 is then fabricated after MMI 610. The  
15   semiconductor die 705 is then be bonded to an AlN carrier and actively aligned on an AlN platform to lens array 710 and thin film filters 640A, 640B, 640C, 640D, etc. The optical performance is then tested.

          Several substeps are preferably performed during  
20   integration, assembly and characterization. These substeps include fabrication of seed array 605 with MMI coupler 610; characterization of performance of device

600, including power, mode shape, spectral  
distribution, & RIN; and iteration of the  
process/design as required. Next, these substeps  
include fabrication of a complete device 600 and  
5 characterization of its performance by assembling it  
together with thin-film filters for stabilization on  
micro-optical bench, and then characterization of  
device 600 performance including power, mode shape,  
spectral distribution, & RIN.

10 Referring again to Figs. 14(a) and 14(b), and as  
discussed hereinabove in the section "6.2.2.5 Fifth  
Embodiment", non-integrated seed and booster amplifier  
waveguides are used to generate high power ASE. The  
seed wavelength generated by discrete seed 505 is not  
15 controlled by a spectral filter nor are the active  
regions of the amplifier waveguides engineered to  
provide an extended gain bandwidth of greater than  
50 nm as described in this preferred embodiment of the  
present invention.

20 The output ASE power in this preferred embodiment  
of the present invention is nearly three times higher  
than the highest known report achieved from a

single-mode semiconductor waveguide (see, for example, Cho, S.H., et al. (2001) "90 mW CW superluminescent output power from single-angled facet-ridge waveguide at 1.5  $\mu\text{m}$ ." Trends in Optics and Photonics Series 31)

5 and more than ten times that of any comparable commercial product (e.g., several telecommunication instrumentation suppliers market broadband single-mode fiber-coupled semiconductor LED sources for use in passive WDM component characterization with output  
10 powers in the range of 0 to 10 mW).

Referring now to Fig. 23, and in a preferred embodiment of the present invention, there is shown a plot 715 of the measured light-verses-current performance obtained using device 600 having a discrete  
15 seed array 605 and booster 615 for ASE generation. In this preferred embodiment of the present invention, more than 250 mW of ASE power is generated by the ASE source 500. The seed input power is approximately 3 mW and the measured ASE spectrum has a full-width  
20 half-maximum (FWHM) of 20 nm.

Referring now to Fig. 24, there is shown the measured ASE spectrum 720 from booster waveguide 615 at



100 mW of output power. Similar spectra output is produced at the maximum output power. The RIN spectrum of this source is less than -140dB/Hz from 100 Hz to beyond 15 GHz.

5

#### 7.0 Modifications

A system and method have been disclosed for amplifying optical signals such as those used in telecommunication systems, HFC-CATV applications, and  
10 other instrumentation and imaging applications. A system and method for producing a high power broadband light source from ASE have also been disclosed, where the high power broadband light source may be used for amplifying optical signals or for other purposes, e.g.,  
15 general instrumentation (including, for example, fiberoptic gyros), imaging (including, for example, medical imaging, and semiconductor analysis applications). While various preferred embodiments have been described and shown, it will be understood  
20 that there is no intent to limit the present invention by such disclosure but, rather, it is intended to cover

all modifications and alternate constructions falling within the spirit and scope of the invention.